Earthquake Resistance Technique by PTMD
(Pendulum Tuned Mass Damper)

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EARTHQUAKE RESISTANCE TECHNIQUE BY PTMD (PENDULUM TUNED MASS DAMPER)

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Abstract: The objective of this thesis is to describe the design, construction, implementation and performance of a prototype adaptive pendulum tuned mass damper (PTMD). Furthermore the thesis aims at demonstrating the performance improvements obtained when the pendulum tuned mass damper (PTMD) parameters are optimized. The study considers the effect of adjusting the PTMD tuned frequency and damping ratio on a two storey test structure subjected to broadband and narrowband excitation. An analytical model of the PTMD for a single-degree-of-freedom (SDOF) structure is used to demonstrate the performance improvements when the PTMD parameters are optimized. The optimized model considers the effects of adjusting the frequency ratio, damping ratio, and mass ratio of the combined system to reduce the maximum deflection dynamic vibration absorber when the structure is subjected to a harmonic excitation force. The analytical model is used to simulate the optimal performance of the PTMD system. The experimental PTMD is capable of identifying the structural vibration modes in real time and tuning to the desired mode. The structural vibration control modes are identified by calculating the windowed power spectral density of the structure's acceleration, followed by peak-picking algorithm to identify the modal frequencies. Tuning is performed by moving the pivot location of the pendulum arm via a tuning frame along a set of rails. The design also allows for changes in the external dampening force. An adjustable damper is attached to the pendulum mass to allow for control of the PTMD damping ratio.

Keywords: pendulum tuned mass damper, dynamic vibration absorber, mass ratio, vibration control, damping ratio.

I. INTRODUCTION

The Wind-induced vibrations impose large demands on structural components and connections for tall structures. Taller, lighter, and more slender modern construction is a consequence of the advances in structural materials, design efficiencies and technologies. Tall structures are susceptible to vibrations due to their flexibility, lack of sufficient inherent structural damping, and the larger wind loads these structures are subjected to due to their height. These demands in many cases lead to considerable discomfort to the occupants, particularly at upper floors. Since the designer has little control over the wind loads, aside from optimization the shape of the structure, the available options to minimize the vibrations include reducing the building’s flexibility or enhancing the vibrational dissipation capacity through increased damping. The flexibility of a structure can be reduced by increasing its stiffness, using larger or a greater number of structural components, resulting in structures with increased weight. Heavier structures consume more materials, require increased construction effort and time, necessitate larger foundations, and are generally more costly. Methods to increase damping in structures are an active area of research. The basic concept of damping is to dissipate vibrational energy through heat, thus reducing the impact of the imposed forces on the structure. One method of mitigating the effects of wind-induced vibrations is through the use of auxiliary damping devices, known as tuned mass dampers TMD.

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II. METHODOLOGY

1. Pendulum Tuned Mass Damper.

The problems associated with the bearings can be eliminated by supporting the mass with cables which allow the system to behave as a pendulum. Shows a simple pendulum attached to a floor. Movement of the floor excites the pendulum. The relative motion of the pendulum produces a horizontal force that opposes the floor motion. This action can be represented by an equivalent SDOF system that is attached to the floor.

- The equation of motion for the horizontal direction is
  \[ T \sin \theta \ Wd \ g - u \ddot{u} + ( ) + d = 0 \]
- Where \( T \) is the tension in the cable
  \[ u_d = L \sin \theta \approx L \theta \]
  \[ T = Wd \]
- The natural frequency of the pendulum is related to by
  \[ \omega_d^2 = \frac{k_{eq}}{mg} = \frac{g}{L} \]
- The natural period of the pendulum is
  \[ T_d = \frac{2 \times 22}{7} \times (L/g) \]

III. TABLE

Table: Type of Structure of PTMD.

<table>
<thead>
<tr>
<th>Sr. No.</th>
<th>Name</th>
<th>Type of Structure</th>
<th>Height</th>
<th>No. Floors</th>
<th>Location</th>
<th>Year Completed</th>
<th>TMD</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>CN Towet Tower</td>
<td>Tower</td>
<td>553m</td>
<td>75</td>
<td>Toronto, Canada</td>
<td>1976</td>
<td>2PTMD Weight= 18 ton</td>
</tr>
<tr>
<td>2</td>
<td>Steel Chimney Chimney</td>
<td>Chimney</td>
<td>90m</td>
<td>-</td>
<td>Bangkok, Thailand</td>
<td>1999</td>
<td>PTMD Frequency= 0.8Hz. Weight= 4ton</td>
</tr>
<tr>
<td>3</td>
<td>Aspire Tower Tower</td>
<td>Tower</td>
<td>300m</td>
<td>36</td>
<td>Doha, Qatar</td>
<td>2007</td>
<td>PTMD Frequency= 0.22 Hz Weight = 140 ton</td>
</tr>
<tr>
<td>4</td>
<td>ShenZhen WuTong Mountain Tower</td>
<td>Tower</td>
<td>198 m</td>
<td>-</td>
<td>ShenZhen, China</td>
<td>2009</td>
<td>PTMD Weight= 10 ton</td>
</tr>
<tr>
<td>5</td>
<td>Taipei 101 Tower</td>
<td>Tower</td>
<td>509.2 m</td>
<td>101</td>
<td>Taipei, Taiwan</td>
<td>2004</td>
<td>PTMD Weight=756 ton</td>
</tr>
</tbody>
</table>

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IV. CONCLUSION

▪ The PTMD presented here is a novel TMD system developed to provide the capability to autonomously tune to the structural frequency while providing control of the external damping to the PTMD mass.

▪ The objective of these tests was to demonstrate the performance improvements over various detuned conditions when the structure is tuned to the structural natural frequency.

▪ The narrowband tests revealed a 7.8% to 17.2% improvement in the measured top floor response when comparing the tuned and off-tuned test conditions.

▪ While the experiment results are certainly positive, they are meant to demonstrate the importance of optimizing the TMD tuning parameters to reduce structural vibrations.

▪ In comparison to passive TMD systems the PTMD will perform as well or better, depending on the disparity between the optimal TMD tuning parameters and the calibrated TMD parameters.

▪ Full size prototype PTMD testing would provide a more clear idea of the obstacles that may emerge if the existing design is to be utilized in a real structure.

▪ The ultimate goal in developing the PTMD is for the technology to become a superior alternative to existing passive TMD technologies.

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REFERENCES


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